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Original article

# NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub>: A low-firing microwave dielectric ceramic with low permittivity and chemical compatibility with silver for LTCC applications

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#### ABSTRACT

Phase formation, crystal structure and dielectric properties of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> ceramics fabricated via a solid state reaction route at relatively low temperatures (780–860 °C) were investigated. NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> crystallizes in a triclinic structure. Dielectric properties were measured based on the Hakki-Coleman post resonator method at microwave frequency. Specially, a specimen sintered at 840 °C demonstrated balanced dielectric properties with a permittivity  $\varepsilon_r=9.72$ , a quality factor  $Q\times f=51,000$  GHz, and a temperature coefficient of resonance frequency  $\tau_f=-84$  ppm/°C. NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> ceramics showed excellent chemical compatibility with Ag metal electrodes. Besides, the thermal stability of resonance frequency was effectively adjusted through formation of composite ceramics between NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> and TiO<sub>2</sub> and a near-zero  $\tau_f$  ~ 1.3 ppm/°C accompanied with  $\varepsilon_r=14.9$  and  $Q\times f=19,600$  GHz was achieved when 50% mol TiO<sub>2</sub> was added. All the merits render NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> a potential candidate for multilayer electronic devices.

#### 1. Introduction

Nowadays, electronic devices have witnessed a constant decrease in the geometrical dimensions of the devices, or in other words, they are being miniaturized. For wireless communication systems, such as a mobile phone, a substantial reduction in sizes (devices or electronic components) have been experienced. The ever-accelerated requirements for miniaturization exert an increasing demand for material exploitation and device design. One direction for device miniaturization is the utilization of high-permittivity ( $\Sigma_r$ ) materials because the size of the dielectric resonator is inversely proportional to the permittivity [1,2]. Nevertheless, the dielectric loss, necessary for noise reduction and controlling the cross-talks, inversely correlates to the dielectric permittivity, which makes the high- $\Sigma_r$  materials practically unfavorable in the high-frequency fields. Moreover, high- $\Sigma_r$  materials generally possess a relatively high temperature coefficient of permittivity that is disadvantageous for the thermal stability of devices.

In addition to exploring high- $\Sigma_r$  materials for miniaturization and

integration, current research interest has been directed to low-temperature co-fired ceramics (LTCC) technology to integrate a versatile mix of passive components such as antennas, filter, resonators, and capacitors within a monolithic bulk module [3–6]. Thus, to achieve cofiring with inner metal electrodes (e.g. Ag), low sintering temperatures (< 961 °C, which is the melting point of Ag) should be satisfied along with chemical compatibility between ceramic matrix and electrodes [7–10].

Generally, the addition of low-melting-point glasses and/or sintering aids proved to be a valid method to develop LTCC systems [11]. However, lowering the sintering temperatures is usually coupled with the deterioration in dielectric properties, especially the quality factor. Within the past two decades, ceramics with intrinsically low densification temperatures have been widely researched, enriching the material systems for LTCC technology. Up till now, a great deal of low-firing ceramics has been reported [12–14]. Those materials with low-melting-point constituents, such as  $B_2O_3$  (450 °C),  $V_2O_5$  (690 °C),  $TeO_2$  (733 °C),  $MoO_3$  (795 °C),  $Bi_2O_3$  (817 °C), tend to have low sintering

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temperatures [5,15–19]. That is because of the mass transfer due to a liquid phase transition. This proves that for state of the art microwave dielectric materials having intrinsically low sintering temperatures and excellent dielectric performances, it is necessary to focus on the materials consisting of low-melting-point constituents.

Recently, an alkaline earth metal vanadate with an alkali  $(NaCa_4V_5O_{17})$  was synthesized and characterized for its crystal structure, spectrum properties, and thermal behavior [20].  $NaCa_4V_5O_{17}$  has a triclinic structure, with 3D frameworks of corner-shared  $VO_4$  tetrahedra that enclose cavities occupied by  $Na^+$  and  $Ca^{2+}$  cations. The single-phase  $NaCa_4V_5O_{17}$  could be obtained after firing it at 600 °C which makes  $NaCa_4V_5O_{17}$  an excellent candidate for microwave dielectric application having low-temperature firing.

In this work,  $NaCa_4V_5O_{17}$  ceramics were prepared via the conventional solid-state reaction route. The microstructure, sintering behaviors and their effects on dielectric properties were studied in details together with the chemical compatibility of  $NaCa_4V_5O_{17}$  with silver.

#### 2. Experimental

#### 2.1. Sample preparation

NaCa $_4$ V $_5$ O $_{17}$  ceramics were prepared via a conventional solid-state method using stoichiometric starting materials: CaCO $_3$ , Na $_2$ CO $_3$  (> 99.95%, Guo-Yao Co., Ltd Shanghai, China) and NH $_4$ VO $_3$  (> 99.9%, Guo-Yao Co., Ltd Shanghai, China). The stoichiometrically weighted powders were mixed through ball-milling in alcohol medium for 6 h. After drying at 120 °C, the resultant powders were calcined at 650 °C for 6 h in air, followed by a second ball milling for 6 h. Green disks were obtained by pressing powder into cylinders (10 mm in diameter and 6 mm in thickness) under a pressure of 80 MPa with polyvinyl alcohol (PVA, 10 vol.%) as s binder. NaCa $_4$ V $_5$ O $_{17}$  pellets were sintered at 780–860 °C for 6 h to optimize the sintering behavior. To suppress evaporation of volatile elements, such as sodium and vanadium, NaCa $_4$ V $_5$ O $_{17}$  ceramics were buried in sacrificial powders of the same composition.

## 2.2. Characterization

The phase purity and crystal structure were analyzed using X-ray diffraction (CuKα1, 1.54059 Å, Model X'Pert PRO, PANalytical, Almelo, Holland). The bulk density was determined by the Archimedes' principle. The surface morphologies of the polished and thermal etched surfaces were observed by scanning electron microscope (FE-SEM, Model S4800, Hitachi, Japan) fitted with an Energy Dispersive Spectroscopy (EDS). The precise composition of the sintered samples was determined using X-Ray Fluorescence Spectrometer (ZSX Primus II, Japan). High-resolution transmission electron microscopy (HRTEM) and the corresponding selected area electron diffraction (SAED) were performed with a JEM-2100 F at an accelerating voltage of 200 kV. The relative permittivity  $(\varepsilon_r)$  and quality factor  $(Q \times f)$  were measured via the Hakki-Coleman dielectric resonator method with TE011 mode using a network analyzer (Model N5230A, Agilent Co., Palo Alto, America) and the temperature coefficient of resonant frequency  $(\tau_f)$  was obtained by recording the temperature shifts of the resonance frequency in the temperature range from 25 to 85 °C using a temperature chamber (Delta 9039, Delta Design, San Diego, CA) and the values were calculated as follows:

$$\tau_f(ppm/{}^{o}C) = \frac{f_2 - f_1}{f_1(T_2 - T_1)} \times 10^{6}$$
(1)

where,  $f_1$  and  $f_2$  represent resonant frequencies at temperatures  $T_1$  (25 °C) and  $T_2$  (85 °C), respectively.

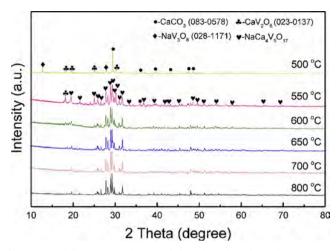


Fig. 1. X-ray diffraction profiles recorded on the calcined powders at various temperatures from 500 to 800  $^{\circ}\text{C}.$ 

#### 3. Results and discussion

Fig. 1 shows the XRD profiles of the powders calcined at various temperatures (ranging from 500 to 800 °C). For the sample fired at 500 °C, three main phases indexed as  $\text{CaCO}_3$  (No. 083-0578),  $\text{CaV}_2\text{O}_6$  (No. 023-0137), and  $\text{NaV}_3\text{O}_8$  (No. 028-1171) were detected. This indicates that at low processing temperatures, the primary chemical reactions is decomposition of raw materials to initiate a chemical reaction forming intermediate phases, which was confirmed from thermal analysis and shown in Supplementary Fig. 1. With increasing calcination temperature,  $\text{NaCa}_4\text{V}_5\text{O}_{17}$  phase began to appear at 550 °C, and eventually became a main phase at 650 °C which kept stable up to 800 °C. Rietveld refinement was performed to determine the crystal structure and to confirm the phase purity based on the powder XRD data collected on the cracked ceramics (sintered at 800 °C).

A structural model with a space group of P-1 was established based on the previous work [20]. The calculated XRD pattern matched well with the observed pattern and shown in Fig. 2. The comparison gives a relatively low difference profiles and acceptable reliability factors of the profile  $R_p = 11.51\%$ , and the weighted profile  $R_{wp} = 9.39\%$ , which verifies the refinement reliability and phase purity of the sample. The lattice parameters were refined as  $a = 6.9368 \, \text{Å}$ ,  $b = 6.9523 \, \text{Å}$ ,  $c = 15.4928 \, \text{Å}$ ,  $a = 84.5550^\circ$ ,  $\beta = 87.2871^\circ$ , and  $\gamma = 86.8512^\circ$ . The refined atomic positions are summarized in Supplementary Table 1. A high resolution transmission electron microscopy (HRTEM) image and

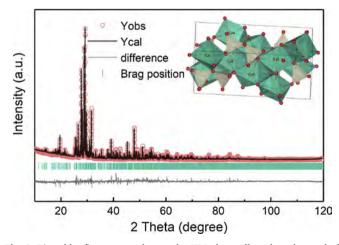


Fig. 2. Rietveld refinement on the powder XRD data collected on the cracked ceramics (sintered at 800 °C) using Fullprof software; the schematic crystal structure of  $NaCa_4V_5O_{17}$  is shown in the inset with grey polyhedra for  $VO_4$ .

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the corresponding selected area electron diffraction (SAED) pattern acquired along the crystallographic [100] direction (Supplementary Fig. 2) further confirmed the triclinic crystal structure. The crystal structure of NaCa $_4$ V $_5$ O $_{17}$  is shown in the inset of Fig. 2, which features a 3D network of corner-shared VO $_4$  tetrahedra with Na and Ca occupying the interstitial sites having seven-coordination and/or six-coordination with oxygen.

X-Ray Fluorescence Spectrometer (XRF) was employed to precisely determine the chemical constitution of NaCa $_4$ V $_5$ O $_{17}$  as oxygen loss in oxides frequently occurs and is represented by the KrÖger–Vink notation:

$$O_0 = 1/2O_2 + V_0^{\bullet \bullet} + 2e^{\bullet}$$
 (2)

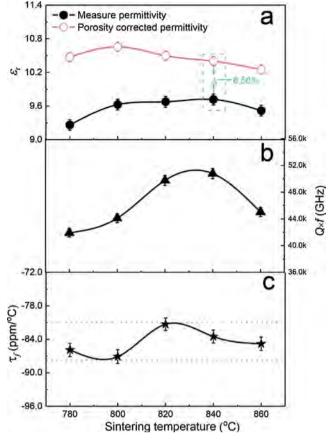
Inevitably, high-temperature firing would induce evaporation of volatile elements, (such as sodium in the present work) and sodium loss accelerates oxygen deficiency to maintain electrical neutrality. The ionization of oxygen vacancies produces the conducting electrons, which would weakly bond with positively charged defects, resulting in another dielectric polarization. XRF analysis revealed mole ratio for Na:Ca:V = 0.227:1:1.123, which deviated from the stoichiometric ratio (0.25:1:1.125), especially for Na source.

The variation in bulk density and relative density as a function of sintering temperature is presented in Fig. 3a. When powder was sintered at 780 °C, the sample had a relatively low bulk density of 2.9 g/cm³ (~92% of relative density), which increased to a maximum density of  $3.03\,\mathrm{g/cm^3}$  (~95.3% of relative density) at 840 °C. Further increase in temperature to 860 °C, however, led to a decline in bulk density to a value of  $3.0\,\mathrm{g/cm^3}$ . The increment in density is believed to be due to the grain growth which squeezes out pores as can be seen in Fig. 3b which shows the SEM image of sample sintered at 840 °C. On the other hand, heterogeneous grain growth with increasing sintering temperature is responsible for the decrease in density and the microstructure showing grain growth is given in Supplementary Figs. 3 and 4.

Fig. 4 presents the variation in microwave dielectric properties as a function of sintering temperature. The relative permittivity increased with increasing sintering temperature and reached a saturated value of 9.72 for the sample sintered at 840 °C. Since, density also exhibited the same trend as permittivity, suggests that the density predominated the relative permittivity of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub>. It is safe to conclude that the relatively small permittivity of air ( $\varepsilon_r$  ~ 1) trapped in the pores also contributed to the permittivity values. In order to remove the effect of porosity, Bosman and Having's equation [21] was used which is presented in Eq. 3:

$$\varepsilon_{corr} = \varepsilon_r (1 + 1.5p) \tag{3}$$

where p is the fractional porosity and  $\varepsilon_{corr}$  is the corrected value. As expected, the calculated  $\varepsilon_{corr}$  values were higher (6–10%) than the



**Fig. 4.** microwave dielectric properties ( $\varepsilon_r$ ,  $Q \times f$ , and  $\tau_f$ ) of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> ceramics sintered at various temperatures from 780 to 860 °C.

measured values and presented in Fig. 4a. Additionally, the theoretical permittivity estimated via the Clausius-Mossotti equation was 8.45, which is also different from the measured value ( $\Delta > 10\%$ ) [22,23]. According to Shannon's report, the lower theoretical permittivity (8.45) of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> indicates that there is another contribution to dielectric polarization that relates to ionic or electronic conductivity or stems from the structural distortion with rattling or compressed cations [22].

Fig. 4b shows the quality factor  $(Q \times f)$  of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> ceramics sintered at various temperatures. For samples sintered at 780 °C, they showed a quality factor  $(Q \times f)$  of 42,000 GHz, which remarkably improved to 51,000 GHz as the sintering temperature rose to 840 °C. Upon further increasing the temperature to 860 °C, the  $Q \times f$  value slightly decreased to 45,000 GHz. A series of factors including intrinsic (such as

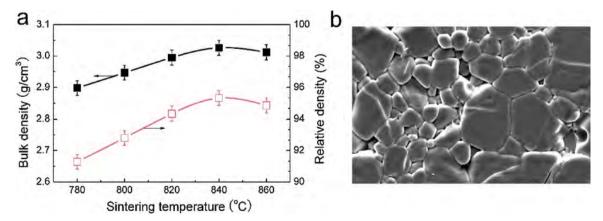


Fig. 3. (a) Density of the sintered NaCa $_4$ V $_5$ O $_{17}$  ceramics at various temperatures from 780 to 860 °C with an increment of 20 °C; (b) SEM image of NaCa $_4$ V $_5$ O $_{17}$  ceramic sintered at 840 °C.

 Table 1

 Microwave dielectric properties of some low-firing vanadates.

Phase	S.T (°C)	$\varepsilon_r$	$Q \times f$ (GHz)	$\tau_f$ (ppm/°C)	Reference
BiVO <sub>4</sub>	925	68	8,000	-243	[27]
$Mg_3(VO_4)_2$	950	9.1	64,142	-93.2	[28]
BiCaVO <sub>5</sub>	820	15.7	55,000	-71	[29]
BiMgVO <sub>5</sub>	820	18.55	86,860	-65	[29]
$Ca_5Co_4(VO_4)_6$	875	10.1	95,200	-63	[30]
LiMoVO <sub>6</sub>	640	13.3	12,460	+101.0	[31]
LiWVO <sub>6</sub>	700	11.5	13,260	163.8	[31]
$NaCa_4V_5O_{17} \\$	840	9.72	51,000	-84	This work

anharmonic lattice vibration) and extrinsic (related to structural imperfection, e.g. point defects, line defects, and plane defects) have been reported to influence the dielectric losses [24–26]. Considering the similar variation trend between quality factor and density versus the sintering temperature, it is rationally determined that density contributes primarily to the dielectric loss.

As shown in Fig. 4c, the temperature coefficient of resonance frequency fluctuated between -87 to -80 ppm/°C for sample sintered between 780 to 860 °C. The weak dependence of  $\tau_f$  on sintering temperature can originate from the fact that no second phase of structural transformation took place over the same temperature range. Table 1 summarizes the sintering temperatures and microwave dielectric properties of some previously researched vanadates with ultra-low sintering temperatures. All the listed vanadates have relatively low sintering temperatures (< 960 °C), rendering their possible utilization in LTCC technology. In comparison, this work possesses low relative permittivity, comparable to Mg<sub>3</sub>(VO<sub>4</sub>)<sub>2</sub>, which is beneficial for highspeed data propagation. The quality factor of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> is much higher than those of BiVO<sub>4</sub> and LiMVO<sub>6</sub> (M = Mo and W), which guarantees its high frequency selectivity. However, the low-firing vanadates usually exhibit non-zero  $\tau_f$  values (either positive or negative), which needs further compensation mechanisms to tune.

Unfortunately, the large negative  $\tau_f$  value makes NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> ceramics impractical, especially in extreme conditions with large temperature variations. Thus, to achieve temperature stability of resonance frequency against temperature, TiO<sub>2</sub> with a positive  $\tau_f$  value (~ + 465 ppm/°C) was chosen as a compensator to form ceramic-ceramic composite [32]. XRD and SEM analysis, given in Fig. 5, confirmed no chemical reaction between TiO<sub>2</sub> and NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub>, which was characterized by distinguishing diffraction peaks and grains with distinct sizes. EDS analysis verified the small grains belong to TiO<sub>2</sub>. As listed in Table 2, TiO<sub>2</sub> addition significantly changed the dielectric properties of the original NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub>. More specifically, the  $\tau_f$  value was shifted

**Table 2** Sintering temperature (S.T.) and microwave dielectric properties of (1-x) NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub>-xTiO<sub>2</sub> composite ceramics.

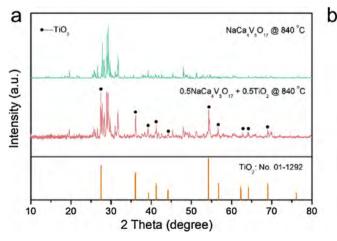
x value	S.T.	$\varepsilon_r$	$\varepsilon_{r\text{cal}}$	$Q \times f$ (GHz)	$\tau_f$ (ppm/°C)	$ au_{ ext{fcal}}$
0	840	9.72	9.72	51,000	-84.3	-84.3
0.1	820	10.5	9.9	45,700	-69.5	-68.9
0.2	820	11.4	10.8	38,800	-57.7	-57.1
0.3	840	12.3	11.7	32,200	-34.6	-34.9
0.4	840	13.1	12.5	25,400	-13.3	-13.7
0.5	840	13.7	13.4	22,500	+3.5	+2.9
0.6	840	14.5	14.1	19,600	+24.3	+23.7

from negative to positive value and a near-zero value of  $+3.5 \, \mathrm{ppm/^oC}$  was achieved with 50 mol%  $\mathrm{TiO_2}$  addition. A composite ceramic with 50 mol%  $\mathrm{TiO_2}$  exhibited balanced dielectric properties with  $\varepsilon_r = 13.7$ ,  $Q \times f = 22,500 \, \mathrm{GHz}$  and  $\tau_f = +3.5 \, \mathrm{ppm/^oC}$ .

In consideration of the relatively low sintering temperature (840 °C) and excellent microwave dielectric properties, NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> can be potentially applicable in low-temperature co-fired ceramics (LTCC) technology, which requires the dielectric materials to be chemically compatible with the electrode materials (silver or aluminum). In order to validate this, NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> cofired with the silver electrode at 840 °C for 30 min and characterized with XRD and SEM for a potential reaction between NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> and silver. Fig. 6 shows the XRD and SEM micrograph of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> cofired with the silver electrode. XRD profiles exhibited the diffraction peaks of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> and silver (as marked by solid circles in Fig. 6a) separately confirming no reaction took place between them. On top of that, distinct grains with different sizes and element contrasts were observed in SEM images. EDS revealed the bright smaller grains in the main ceramic matrix to be silver which further confirms a lack of reaction between silver and NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub>. All these results validate the potential application of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> in LTCC technology.

### 4. Conclusions

NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> ceramics were prepared by solid state reaction at relatively low temperatures (780–860 °C). Thermal analysis and X-ray diffraction patterns confirmed the formation of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> at 650 °C. Rietveld refinement verified the phase purity of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> with a triclinic structure P-1. SEM images show that dense ceramics with homogenous microstructure were developed. Combined dielectric properties were achieved in the sample sintered at 840 °C with  $\varepsilon_r = 9.72$ ,  $Q \times f = 51,000$  GHz, and  $\tau_f = -84$  ppm/°C. Chemical compatibility with Ag of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> ceramics was also determined based on XRD



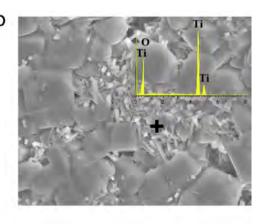


Fig. 5. (a) XRD patterns and (b) SEM micrograph of 0.5NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> + 0.5TiO<sub>2</sub> composite ceramic sintered at 840 °C (EDS analysis of TiO<sub>2</sub> is shown in the inset of Fig. 5b).

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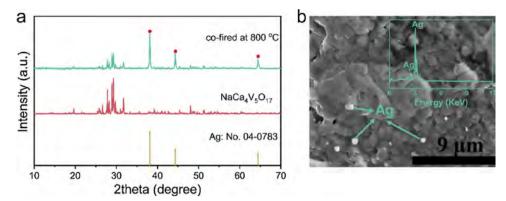


Fig. 6. (a) XRD and (b) SEM micrograph of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> cofired with silver electrode at 840 °C (EDS analysis of Ag is shown in the inset of Fig. 6b).

analysis. Besides, several composite ceramics in the (1-x)NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub>-xTiO<sub>2</sub> system were synthesized with an attempt to adjust the thermal stability of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub>. Effectively, a near-zero  $\tau_f$   $^{\sim}$  +3.5 ppm/ $^{\circ}$ C was accessible in the composite with 50% mol TiO<sub>2</sub> accompanied with  $\varepsilon_r$  = 13.7 and  $Q \times f$  = 22,500 GHz. The intrinsic low sintering temperature, low permittivity along with chemical compatibility with Ag renders the possible application of NaCa<sub>4</sub>V<sub>5</sub>O<sub>17</sub> in multilayer electronic devices.

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